Preliminary Mathematics of Geometric Modeling (2)

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Representation of Curves and Surfaces

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Parametric Form

$$x = x(t), \quad y = y(t)$$

where
$$t_1 \le t \le t_2$$

x(t) and y(t) are assumed to be continuous with a sufficient number of continuous derivatives

• Vector-Valued Parametric Form $\mathbf{r} = \mathbf{r}(t)$

• Implicit Form

$$f(x,y) = 0$$

• Linear (line): f(x,y) = ax+by+c = 0

• Quadric (Conic sections): $ax^2 + 2bxy + cy^2 + 2dx + 2ey + h = 0$

• Explicit Form

$$y = F(x)$$
 or $x = G(y)$

 A special case of parametric and implicit forms

Special parametric form if

$$\frac{dx}{dt} \neq 0$$
 or $\frac{dy}{dt} \neq 0$

is satisfied at least locally.

• Special implicit form if $\frac{\partial f}{\partial y} \neq 0$ or $\frac{\partial f}{\partial x} \neq 0$

is satisfied at least locally.

 A planar curve can also be expressed as an intersection curve between a plane and a surface

Example of Planar Curves



Cubic curve with a single loop, a node, and two ends asymptotic to the same line

$$\mathbf{r}(t) = \left(\frac{3t}{1+t^3}, \frac{3t^2}{1+t^3}\right)^T$$
$$-\infty < t < \infty \quad (t \neq -1)$$

Parametric form $f(x,y) = x^3 + y^3 - 3xy = 0$

Implicit form

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Representation of Space Curves

 The parametric representation of space curves

$$\label{eq:constraint} \begin{split} x = x(t), \quad y = y(t), \quad z = z(t) \\ \text{where} \end{split}$$

$$t_1 \le t \le t_2$$

Representation of Space Curves

- The implicit representation of space curves
 - intersection curve between two implicit surfaces

$$f(x, y, z) = 0 \cap g(x, y, z) = 0$$

 intersection curve between parametric and implicit surfaces

$$\mathbf{r} = \mathbf{r}(u, v) \ \cap \ f(x, y, z) = 0$$

Representation of Space Curves

- The implicit representation of space curves
 - intersection curve between two parametric surfaces

$$\mathbf{r} = \mathbf{p}(\sigma, t) \ \cap \ \mathbf{r} = \mathbf{q}(u, v)$$

Representation of Space Curves

 The explicit representation of space curves

$$y = Y(x), \quad z = Z(x)$$

It is hold at least locally when

- Parametric form: $\frac{dx}{dt} \neq 0$
- Implicit form: $\frac{\partial f}{\partial y} \frac{\partial g}{\partial z} \frac{\partial f}{\partial z} \frac{\partial g}{\partial y} \neq 0$

Representation of Space Curves

 The explicit representation of space curves

$$y = Y(x), \quad z = Z(x)$$

The explicit equation for the space curve can be expressed as an intersection curve of two cylinders projecting the curve onto *xy* and *xz* planes.

Parametric Form

$$x = x(u, v), \quad y = y(u, v), \quad z = z(u, v)$$

where

$$u_1 \le u \le u_2, \ v_1 \le v \le v_2$$

Note: the functions x(u,v), y(u,v) and z(u,v)are continuous and possess a sufficient number of continuous partial derivatives

Parametric form as vector-valued function

$$\mathbf{r} = \mathbf{r}(u, v)$$

• Implicit form: an *implicit surface* is defined as the locus of points whose coordinates (*x*,*y*,*z*) satisfy an equation of the form

•
$$f(x,y,z)$$
 is linear: $f(x,y,z) = 0$

f(x,y,z) is quadratic in the variables x,y,z:
 quadratic surface

 $ax^{2} + by^{2} + cz^{2} + dxy + eyz + hxz + kx + ly + mz + n = 0$

• Quadratic surfaces:

- The natural quadrics, sphere, circular cone and circular cylinder: widely used in mechanical design and CAD/CAM systems
- Result from standard manufacturing operations: rolling, turning(+), filleting(-),drilling and milling
- 80-85% of mechanical parts were adequately represented by planes and cylinders, while 90-95% were modeled with the addition of cones. (Univ. of Rochester, in the mid 1970's)



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Explicit Form

$$z = F(x, y)$$

- From implicit form: locally $\frac{\partial f}{\partial z} \neq 0$
- From parametric form: locally $\frac{\partial x}{\partial u}\frac{\partial y}{\partial v} \frac{\partial x}{\partial v}\frac{\partial y}{\partial u} \neq 0$
- z=F(x,y): x=u, y=v, z=f(u,v)
 explicit form is special case of parametric form.

 Example: hyperbolic paraboloid surface patch parametric form:

 $x = u + v, \quad y = u - v, \quad z = u^2 - v^2, \quad 0 \le u, v \le 1$ explicit form: u=(x+y)/2, v=(x-y)/2

$$z = xy, \quad 0 \le x + y \le 2, \ 0 \le x - y \le 2$$

Summary

Representations of curves and surfaces

Geometry	Parametric	Implicit	Explicit
Plane	x = x(t), y = y(t)	f(x,y) = 0 or	y = F(x)
curves	$t_1 \le t \le t_2$	$\mathbf{r} = \mathbf{r}(u, v) \cap \text{plane}$	
Space	$x = x(t), \ y = y(t),$	$f(x,y,z) = 0 \cap g(x,y,z) = 0$	$y = Y(x) \cap $
curves	$z = z(t), t_1 \le t \le t_2$	or $\mathbf{r} = \mathbf{r}(u, v) \cap f(x, y, z) = 0$	z = Z(x)
		or $\mathbf{r} = \mathbf{p}(\sigma, t) \cap \mathbf{r} = \mathbf{q}(u, v)$	
Surfaces	x = x(u, v),	f(x, y, z) = 0	z = F(x, y)
	y = y(u, v),		
	z = z(u, v),		
	$u_1 \le u \le u_2,$		
	$v_1 \le v \le v_2$		

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	Disadvantages	
Explicit	Implicit	Parametric
 Infinite slopes are impossible if f(x) is a polynomial. Axis dependent (difficult to transform). Closed and multivalued curves are difficult to represent. 	 Difficult to fit and manipulate free form shapes. Axis dependent. Complex to trace. 	• High flexibility compli- cates intersections and point classification.
	Advantages	
Explicit	Implicit	Parametric
• Easy to trace.	 Closed and multival- ued curves and infinite slopes can be repre- sented. Point classification (solid modeling, in- terference check) is easy. 	 Closed and multival- ued curves and infinite slopes can be repre- sented. Axis independent (easy to transform).
	• Intersections/offsets can be represented.	 Easy to generate composite curves. Easy to trace. Easy in fitting and manipulating free-form shapes.

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Summary

- The parametric form is the most versatile method among the three and the explicit is the least
- The explicit form can always be easily converted to parametric form
- Conversion between parametric form and implicit form

Differential Geometry of Curves

- Arc length and tangent vector
- Principal normal and curvature
- Binormal vector and torsion
- Frenet-Serret formulae



Parametric curve $\mathbf{r}=\mathbf{r}(t)$ Segment between PQ $P(\mathbf{r}(t)) \ Q(\mathbf{r}(t+\Delta t))$ Its arc length Δs

$$\Delta s \simeq |\Delta \mathbf{r}| = |\mathbf{r}(t + \Delta t) - \mathbf{r}(t)|$$

$$= \left| \frac{d\mathbf{r}}{dt} \Delta t + \frac{d^2 \mathbf{r}}{dt^2} (\Delta t)^2 \right| \simeq \left| \frac{d\mathbf{r}}{dt} \right| \Delta t$$

$$ds = \left|\frac{d\mathbf{r}}{dt}\right| dt = |\dot{\mathbf{r}}| dt = \sqrt{\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}} dt$$

• Arc length between $\mathbf{r}(t_0)$ and $\mathbf{r}(t)$

$$s(t) = \int_{t_o}^t ds = \int_{t_o}^t \sqrt{\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}} dt = \int_{t_o}^t \sqrt{\dot{x}^2(t) + \dot{y}^2(t) + \dot{z}^2(t)} dt$$

Tangent vector <u>dr/dt</u> : <u>r</u>erivative about <u>t</u>

$$|\dot{\mathbf{r}}| = rac{ds}{dt}$$

 $\mathbf{\dot{r}}$ is called parametric speed

• Useful formulae of the derivatives (s / t)

$$\begin{split} \dot{s} &= \frac{ds}{dt} = |\dot{\mathbf{r}}| = \sqrt{\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}} \\ \ddot{s} &= \frac{d\dot{s}}{dt} = \frac{\dot{\mathbf{r}} \cdot \ddot{\mathbf{r}}}{\sqrt{\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}}} , \\ \ddot{s} &= \frac{d\dot{s}}{dt} = \frac{\dot{\mathbf{r}} \cdot \ddot{\mathbf{r}}}{\sqrt{\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}}} , \\ \vdots &= \frac{d\ddot{s}}{dt} = \frac{(\dot{\mathbf{r}} \cdot \dot{\mathbf{r}})(\dot{\mathbf{r}} \cdot \overset{\cdots}{\mathbf{r}} + \ddot{\mathbf{r}} \cdot \ddot{\mathbf{r}}) - (\dot{\mathbf{r}} \cdot \ddot{\mathbf{r}})^2}{(\dot{\mathbf{r}} \cdot \dot{\mathbf{r}})^{\frac{3}{2}}} \end{split} \qquad t'' = \frac{dt'}{ds} = -\frac{\dot{\mathbf{r}} \cdot \ddot{\mathbf{r}}}{(\dot{\mathbf{r}} \cdot \dot{\mathbf{r}})^2} , \\ t''' &= \frac{dt'}{ds} = -\frac{(\ddot{\mathbf{r}} \cdot \ddot{\mathbf{r}} + \dot{\mathbf{r}} \cdot \ddot{\mathbf{r}})(\dot{\mathbf{r}} \cdot \dot{\mathbf{r}}) - 4(\dot{\mathbf{r}} \cdot \ddot{\mathbf{r}})^2}{(\dot{\mathbf{r}} \cdot \dot{\mathbf{r}})^{\frac{3}{2}}} \end{split}$$

• Derivative about arc length: \mathbf{r}' $\mathbf{t} = \frac{\dot{\mathbf{r}}}{|\dot{\mathbf{r}}|} = \frac{\frac{d\mathbf{r}}{dt}}{\frac{ds}{dt}} = \frac{d\mathbf{r}}{ds} \equiv \mathbf{r}'$

It is a unit vector

• Definition: A regular (ordinary) point *P* on a parametric curve $\mathbf{r}=\mathbf{r}(t)=(x(t),y(t),z(t))^T$ is defined as a point where $|\dot{\mathbf{r}}(t)| \neq 0$. A point which is not a regular point is called a singular point.

- Parameter *t* and Arc length parameter *s*
 - t: arbitrary speed
 - s: unit speed



When parametric speed does not vary significantly, points with uniformly spaced parameter values are nearly uniformly spaced along a parametric curve

- Parameter *t* and Arc length parameter *s*
 - Every regular curve has an arc length parametrization
 - In practice it is very difficult to find it analytically, due to the fact that it is hard to integrate analytically
 - Pythagorean hodograph (PH) curves form a class of special planar polynomial curves whose parametric speed is a polynomial

 Tangent vector of implicit planar curve • f(x,y)=0 total differentiation

$$df = f_x dx + f_y dy = 0$$

by assuming $f_y \neq 0$ $\frac{dy}{dx} = -\frac{f_y}{f_y}$

$$\frac{ly}{lx} = -\frac{f_x}{f_y}$$

Unit tangent vector :

$$\mathbf{t} = \pm \frac{(f_y, -f_x)^T}{\sqrt{f_x^2 + f_y^2}}$$

- Tangent vector of implicit space curve
 - Curve: $f(x,y,z)=0 \cap g(x,y,z)=0$
 - Gradient vector operator: $\nabla = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right)^T$

• Unit tangent vector :

$$\mathbf{t} = \pm \frac{\nabla f \times \nabla g}{|\nabla f \times \nabla g|}$$

- Example $\mathbf{r}(t) = (t^2, t^3)^T$
 - Parametric speed $|\dot{\mathbf{r}}(t)| = \sqrt{t^2(4+9t^2)}$
 - r(0) is a singular point
 - Implicit form: f(x, y) = x³−y² = 0
 (0,0) is a singular point since f(0,0) = f_x(0,0) = f_y(0,0) = 0
Arc length and tangent vector



A singular point occurs on a semi-cubical parabola in the form of a cusp

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r(s): an arc length parametrized curve
 r'(s) unit tangent vector

$$\mathbf{r}' \cdot \mathbf{r}' = 1 \quad \Longrightarrow \quad \mathbf{r}' \cdot \mathbf{r}'' = 0$$

 $\mathbf{r}''(s)$ is orthogonal to $\mathbf{r}'(s)$ $\mathbf{r}''(s) = \lim_{\Delta s \to 0} \frac{\mathbf{r}'(s + \Delta s) - \mathbf{r}'(s)}{\Delta s}$



Derivation of the normal vector of a curve

$$\mathbf{r}''(s) = \lim_{\Delta s \to 0} \frac{\mathbf{r}'(s + \Delta s) - \mathbf{r}'(s)}{\Delta s}$$

$$\mathbf{n} = \frac{\mathbf{r}''(s)}{|\mathbf{r}''(s)|} = \frac{\mathbf{t}'(s)}{|\mathbf{t}'(s)|}$$

n: unit principal normal vector

The plane determined by $\mathbf{t}(s)$ and $\mathbf{n}(s)$ is called osculating plane



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• Calculation of $|\mathbf{r}''(s)|$

$$|\mathbf{r}'(s + \Delta s) - \mathbf{r}'(s)| = \Delta \theta \cdot 1 = \Delta \theta$$

$$\mathbf{r}''(s)| = \lim_{\Delta s \to 0} \frac{\Delta \theta}{\Delta s} = \lim_{\Delta s \to 0} \frac{\Delta \theta}{\varrho \Delta \theta} = \frac{1}{\varrho} \equiv \kappa$$

Q : radius of curvature*κ* : curvature

Curvature vector

$$\mathbf{k} = \mathbf{r}'' = \mathbf{t}' = \kappa \mathbf{n}$$

- measures the rate of change of the tangent along the curve
- It is the same as r["](s) provided defining κ is nonnegative

 Curvature for arbitrary speed curve (nonarc-length parametrized)

$$\begin{split} \dot{\mathbf{r}} &= \frac{d\mathbf{r}}{ds} \frac{ds}{dt} = \mathbf{t}v ,\\ \ddot{\mathbf{r}} &= \frac{d}{dt} [\mathbf{t}v] = \frac{d\mathbf{t}}{ds} v^2 + \mathbf{t} \frac{dv}{dt} = \kappa \mathbf{n}v^2 + \mathbf{t} \frac{dv}{dt}\\ \dot{\mathbf{r}} &\times \ddot{\mathbf{r}} = \kappa v^3 \mathbf{t} \times \mathbf{n} \end{split}$$

$$\kappa = \frac{|\dot{\mathbf{r}} \times \ddot{\mathbf{r}}|}{|\dot{\mathbf{r}}|^3}$$

- Curvature for the planar curve
 - Give the curvature κ a sign by defining the normal vector such that (t,n,e_z) form a righthanded screw

 $\mathbf{e}_{z} = (0, 0, 1)^{T}$

 The point where the curvature changes sign is called an *inflection point*



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The unit normal vector of the plane curve

$$\mathbf{n} = \mathbf{e}_z \times \mathbf{t} = \frac{(-\dot{y}, \dot{x})^T}{\sqrt{\dot{x}^2 + \dot{y}^2}}$$

• The curvature of the plane curve

$$\kappa = \frac{(\dot{\mathbf{r}} \times \ddot{\mathbf{r}}) \cdot \mathbf{e}_z}{v^3} = \frac{\dot{x}\ddot{y} - \dot{y}\ddot{x}}{(\dot{x}^2 + \dot{y}^2)^{\frac{3}{2}}}$$

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 The unit principal normal vector for planar implicit curves (2D)

Unit tangent vector

$$\mathbf{t} = \pm \frac{(f_y, -f_x)^T}{\sqrt{f_x^2 + f_y^2}}$$

Unit principal normal vector

$$\mathbf{n} = \mathbf{e}_z \times \mathbf{t} = \frac{(f_x, f_y)^T}{\sqrt{f_x^2 + f_y^2}} = \frac{\nabla f}{|\nabla f|}$$

The curvature for planar implicit curves

• The curvature for planar implicit curves $\frac{d}{ds} = \frac{1}{|\nabla f|} \left(f_y \frac{\partial}{\partial x} - f_x \frac{\partial}{\partial y} \right)$

$$\left(\frac{dx}{ds}, \frac{dy}{ds}\right)^T = \mathbf{t} = \pm \frac{(f_y, -f_x)^T}{\sqrt{f_x^2 + f_y^2}}$$

$$\kappa = -\frac{f_{xx}f_y^2 - 2f_{xy}f_xf_y + f_x^2f_{yy}}{(f_x^2 + f_y^2)^{\frac{3}{2}}}$$

• The curvature for space implicit curves $\frac{d}{ds} = \frac{1}{|\boldsymbol{\alpha}|} \left(\alpha_1 \frac{\partial}{\partial x} + \alpha_2 \frac{\partial}{\partial y} + \alpha_3 \frac{\partial}{\partial z} \right)$

where

$$\boldsymbol{\alpha} = (\alpha_1, \alpha_2, \alpha_3) = \nabla f \times \nabla g$$
$$\alpha_1 = \frac{\partial f}{\partial y} \frac{\partial g}{\partial z} - \frac{\partial g}{\partial y} \frac{\partial f}{\partial z}$$
$$\alpha_2 = \frac{\partial g}{\partial x} \frac{\partial f}{\partial z} - \frac{\partial f}{\partial x} \frac{\partial g}{\partial z}$$
$$\alpha_3 = \frac{\partial f}{\partial x} \frac{\partial g}{\partial y} - \frac{\partial g}{\partial x} \frac{\partial f}{\partial y}$$

$$\frac{d}{ds} = \frac{1}{|\boldsymbol{\alpha}|} \left(\alpha_1 \frac{\partial}{\partial x} + \alpha_2 \frac{\partial}{\partial y} + \alpha_3 \frac{\partial}{\partial z} \right)$$
$$|\boldsymbol{\alpha}|\mathbf{t} = \boldsymbol{\alpha}$$
$$\frac{d|\boldsymbol{\alpha}|\mathbf{t}}{ds} = \frac{1}{|\boldsymbol{\alpha}|} \left(\alpha_1 \frac{\partial \boldsymbol{\alpha}}{\partial x} + \alpha_2 \frac{\partial \boldsymbol{\alpha}}{\partial y} + \alpha_3 \frac{\partial \boldsymbol{\alpha}}{\partial z} \right)$$
$$\ddot{\mathbf{r}} = \frac{d}{dt} [\mathbf{t}v] = \frac{d\mathbf{t}}{ds} v^2 + \mathbf{t} \frac{dv}{dt} = \kappa \mathbf{n}v^2 + \mathbf{t} \frac{dv}{dt}$$

$$|\boldsymbol{\alpha}|^{2}\kappa\mathbf{n}+|\boldsymbol{\alpha}||\boldsymbol{\alpha}|'\mathbf{t}=\left(lpha_{1}rac{\partial \boldsymbol{\alpha}}{\partial x}+lpha_{2}rac{\partial \boldsymbol{\alpha}}{\partial y}+lpha_{3}rac{\partial \boldsymbol{\alpha}}{\partial z}
ight)$$

Cross product with

$$|\boldsymbol{\alpha}|^{3}\kappa\mathbf{b} = \boldsymbol{\alpha} \times \left(\alpha_{1}\frac{\partial\boldsymbol{\alpha}}{\partial x} + \alpha_{2}\frac{\partial\boldsymbol{\alpha}}{\partial y} + \alpha_{3}\frac{\partial\boldsymbol{\alpha}}{\partial z}\right)$$

Thus

$$\kappa = \frac{\left| \boldsymbol{\alpha} \times \left(\alpha_1 \frac{\partial \boldsymbol{\alpha}}{\partial x} + \alpha_2 \frac{\partial \boldsymbol{\alpha}}{\partial y} + \alpha_3 \frac{\partial \boldsymbol{\alpha}}{\partial z} \right) \right|}{|\boldsymbol{\alpha}|^3}$$

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Define a unit binormal vector b

$$\mathbf{b} = \mathbf{t} imes \mathbf{n}$$

- (t,n.b) form a right-handed screw $b = t \times n$ $t = n \times b$ $n = b \times t$
 - Normal plane: (n,b)
 - Rectifying plane: (**b**,**t**)
 - Osculating plane: (t,n)

Binomal for arbitrary speed parameter *t*

$$\mathbf{b} = rac{\dot{\mathbf{r}} imes \ddot{\mathbf{r}}}{|\dot{\mathbf{r}} imes \ddot{\mathbf{r}}|}$$



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 Torsion: measures how much the curve deviates from the osculating plane

$$\mathbf{b}' = \frac{d}{ds}(\mathbf{t} \times \mathbf{n}) = \frac{d\mathbf{t}}{ds} \times \mathbf{n} + \mathbf{t} \times \frac{d\mathbf{n}}{ds} = \mathbf{t} \times \mathbf{n}' - - -$$
$$\mathbf{t}' = \kappa \mathbf{n}$$

$$\mathbf{n} \cdot \mathbf{n} = 1 \implies \mathbf{n} \cdot \mathbf{n}' = 0 \implies \mathbf{n}' \text{ is parallel to the rectifying plane (b,t)}$$

 $\mathbf{n}' = \mu \mathbf{t} + \tau \mathbf{b}$

$$\mathbf{b}' = \mathbf{t} \times (\mu \mathbf{t} + \tau \mathbf{b}) = \tau \mathbf{t} \times \mathbf{b} = -\tau \mathbf{b} \times \mathbf{t} = -\tau \mathbf{n}$$

Torsion for arc length parameter

$$\tau = -\mathbf{n} \cdot \mathbf{b}' = -\frac{\mathbf{r}''}{\kappa} \cdot \left(\mathbf{r}' \times \frac{\mathbf{r}''}{\kappa}\right)' = -\frac{\mathbf{r}''}{\kappa} \cdot \left(\mathbf{r}' \times \frac{\mathbf{r}'''}{\kappa}\right) = \frac{(\mathbf{r}'\mathbf{r}''\mathbf{r}''')}{\mathbf{r}'' \cdot \mathbf{r}''}$$

Torsion for arbitrary speed parameter

$$\tau = \frac{(\dot{\mathbf{r}}\ddot{\mathbf{r}} \ \overset{\cdots}{\mathbf{r}})}{(\dot{\mathbf{r}} \times \ddot{\mathbf{r}}) \cdot (\dot{\mathbf{r}} \times \ddot{\mathbf{r}})}$$

- Geometric interpretation of torsion
 - τ > 0 : the rotation of the osculating plane is in the direction of a right-handed screw moving in the direction of t as s increases
 - τ < 0 : the rotation of the osculating plane is in the direction of a left-handed screw moving in the direction of t as s increases

•
$$\tau \equiv 0$$
 : planar curve

• Binormal vector for space implicit curve

$$\mathbf{b} = \frac{\boldsymbol{\alpha} \times \left(\alpha_1 \frac{\partial \boldsymbol{\alpha}}{\partial x} + \alpha_2 \frac{\partial \boldsymbol{\alpha}}{\partial y} + \alpha_3 \frac{\partial \boldsymbol{\alpha}}{\partial z}\right)}{|\boldsymbol{\alpha} \times \left(\alpha_1 \frac{\partial \boldsymbol{\alpha}}{\partial x} + \alpha_2 \frac{\partial \boldsymbol{\alpha}}{\partial y} + \alpha_3 \frac{\partial \boldsymbol{\alpha}}{\partial z}\right)|}$$

 Torsion of space implicit curve $\xrightarrow{d} \frac{d}{ds} = \frac{1}{|\boldsymbol{\alpha}|} \left(\alpha_1 \frac{\partial}{\partial x} + \alpha_2 \frac{\partial}{\partial y} + \alpha_3 \frac{\partial}{\partial z} \right)$ $--|\boldsymbol{\alpha}|^{3}\kappa\mathbf{b} = \boldsymbol{\alpha}\times\left(\alpha_{1}\frac{\partial\boldsymbol{\alpha}}{\partial x} + \alpha_{2}\frac{\partial\boldsymbol{\alpha}}{\partial u} + \alpha_{3}\frac{\partial\boldsymbol{\alpha}}{\partial z}\right)$ $\frac{d}{ds}(|\boldsymbol{lpha}|^3\kappa\mathbf{b}) =$ $\frac{1}{|\boldsymbol{\alpha}|} \left(\alpha_1 \frac{\partial}{\partial x} + \alpha_2 \frac{\partial}{\partial y} + \alpha_3 \frac{\partial}{\partial z} \right) \left(\boldsymbol{\alpha} \times \left(\alpha_1 \frac{\partial \boldsymbol{\alpha}}{\partial x} + \alpha_2 \frac{\partial \boldsymbol{\alpha}}{\partial y} + \alpha_3 \frac{\partial \boldsymbol{\alpha}}{\partial z} \right) \right)$

$$-|\boldsymbol{\alpha}|^{6}\kappa^{2}\tau = \left(\alpha_{1}\frac{\partial\boldsymbol{\alpha}}{\partial x} + \alpha_{2}\frac{\partial\boldsymbol{\alpha}}{\partial y} + \alpha_{3}\frac{\partial\boldsymbol{\alpha}}{\partial z}\right)$$
$$\cdot \left(\alpha_{1}\frac{\partial}{\partial x} + \alpha_{2}\frac{\partial}{\partial y} + \alpha_{3}\frac{\partial}{\partial z}\right)\left(\boldsymbol{\alpha}\times\left(\alpha_{1}\frac{\partial\boldsymbol{\alpha}}{\partial x} + \alpha_{2}\frac{\partial\boldsymbol{\alpha}}{\partial y} + \alpha_{3}\frac{\partial\boldsymbol{\alpha}}{\partial z}\right)\right)$$



Circular helix with a = 2, b = 3 for $0 \le t \le 6 \pi$

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The parametric speed
$$|\dot{\mathbf{r}}(t)| = \sqrt{a^2 + b^2} \equiv c$$

Arc length $s(t) = \int_0^t |\dot{\mathbf{r}}| dt = \int_0^t \sqrt{a^2 + b^2} dt = ct$

Arc length parameterization

$$\mathbf{r} = (a \cos \frac{s}{c}, a \sin \frac{s}{c}, \frac{bs}{c})^T$$

Derivatives to arc length $\mathbf{r}'(s) = \left(-\frac{a}{c}\sin\frac{s}{c}, \frac{a}{c}\cos\frac{s}{c}, \frac{b}{c}\right)^T$

$$\mathbf{r}''(s) = \left(-\frac{a}{c^2}\cos\frac{s}{c}, -\frac{a}{c^2}\sin\frac{s}{c}, 0\right)^T$$

$$\mathbf{r}^{\prime\prime\prime}(s) = \left(\frac{a}{c^3}\sin\frac{s}{c}, -\frac{a}{c^3}\cos\frac{s}{c}, 0\right)^T$$

Curvature and torsion

$$\kappa^{2} = \mathbf{r}'' \cdot \mathbf{r}'' = \frac{a^{2}}{c^{4}} \left(\cos^{2} \frac{s}{c} + \sin^{2} \frac{s}{c} \right) = \frac{a^{2}}{c^{4}} = constant ,$$

$$\tau = \frac{(\mathbf{r}'\mathbf{r}''\mathbf{r}''')}{\mathbf{r}'' \cdot \mathbf{r}''} = \frac{(\mathbf{r}'\mathbf{r}''\mathbf{r}''')}{\kappa^{2}} = \frac{c^{4}}{a^{2}} \begin{vmatrix} -\frac{a}{c} \sin \frac{s}{c} & \frac{a}{c} \cos \frac{s}{c} & \frac{b}{c} \end{vmatrix}$$

$$-\frac{a}{c^{2}} \cos \frac{s}{c} - \frac{a}{c^{2}} \sin \frac{s}{c} & 0 \end{vmatrix}$$

$$\frac{a}{c^{3}} \sin \frac{s}{c} - \frac{a}{c^{3}} \cos \frac{s}{c} & 0 \end{vmatrix}$$

$$= \frac{c^4}{a^2} \frac{b}{c} \frac{a^2}{c^5} \left(\cos^2 \frac{s}{c} + \sin^2 \frac{s}{c} \right) = \frac{b}{c^2} = constant$$

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We have known $\mathbf{t}' = \kappa \mathbf{n}$ $\mathbf{b}' = -\tau \mathbf{n}$ $\mathbf{n}' = (\mathbf{b} \times \mathbf{t})' = \mathbf{b}' \times \mathbf{t} + \mathbf{b} \times \mathbf{t}'$ $= -\tau \mathbf{n} \times \mathbf{t} + \mathbf{b} \times (\kappa \mathbf{n}) = -\kappa \mathbf{t} + \tau \mathbf{b}$

For the arc length parameter

$$\begin{pmatrix} \mathbf{t}' \\ \mathbf{n}' \\ \mathbf{b}' \end{pmatrix} = \begin{pmatrix} 0 & \kappa & 0 \\ -\kappa & 0 & \tau \\ 0 & -\tau & 0 \end{pmatrix} \begin{pmatrix} \mathbf{t} \\ \mathbf{n} \\ \mathbf{b} \end{pmatrix}$$

Frenet-Serret formulae

Intrinsic equations of the curve

$$\kappa \,=\, \kappa(s), \; \tau \,=\, \tau(s)$$

They totally decide the shape of curve except for a rigid transformation!

For the arbitrary speed parameter



A circular helix $\mathbf{r}(t) = (a \cos t, a \sin t, bt)^T$



A circular helix $\mathbf{r}(t) = (a \cos t, a \sin t, bt)^T$ Arc length parametrization

$$\mathbf{r} = (a \cos \frac{s}{c}, a \sin \frac{s}{c}, \frac{bs}{c})^T$$

Intrinsic equations

$$\kappa(s) = \frac{a}{c^2}, \ \tau(s) = \frac{b}{c^2}$$
$$c = \sqrt{a^2 + b^2}$$

Frenet-Serret equations $\frac{d\mathbf{t}}{ds} = \frac{a}{c^2}\mathbf{n}, \quad \frac{d\mathbf{n}}{ds} = -\frac{a}{c^2}\mathbf{t} + \frac{b}{c^2}\mathbf{b}, \quad \frac{d\mathbf{b}}{ds} = -\frac{b}{c^2}\mathbf{n}$

Differentiate the first equation twice and the second equation once

$$\frac{d^2\mathbf{t}}{ds^2} = \frac{a}{c^2}\frac{d\mathbf{n}}{ds}, \qquad \frac{d^3\mathbf{t}}{ds^3} = \frac{a}{c^2}\frac{d^2\mathbf{n}}{ds^2}, \qquad \frac{d^2\mathbf{n}}{ds^2} = -\frac{a}{c^2}\frac{d\mathbf{t}}{ds} - \frac{b^2}{c^4}\mathbf{n}$$

Eliminating
$$\mathbf{n}, \frac{d\mathbf{n}}{ds}, \frac{d^2\mathbf{n}}{ds^2}$$

$$\frac{d^4\mathbf{r}}{ds^4} + \frac{1}{c^2}\frac{d^2\mathbf{r}}{ds^2} = 0$$

The general solution is $\mathbf{r}(s) = \mathbf{C}_1 + \mathbf{C}_2 s + \mathbf{C}_3 \cos \frac{s}{c} + \mathbf{C}_4 \sin \frac{s}{c}$
Frenet-Serret formulae: example

Given initial conditions

$$\mathbf{r}(0) = (a, 0, 0)^{T}$$

$$\mathbf{C}_{1} = (0, 0, 0)^{T}$$

$$\mathbf{r}'(0) = \left(0, \frac{a}{c}, \frac{b}{c}\right)^{T}$$

$$\mathbf{C}_{2} = \left(0, 0, \frac{b}{c}\right)$$

$$\mathbf{r}''(0) = \left(-\frac{a}{c^{2}}, 0, 0\right)^{T}$$

$$\mathbf{C}_{3} = (a, 0, 0)^{T}$$

$$\mathbf{r}'''(0) = \left(0, -\frac{a}{c^{3}}, 0\right)^{T}$$

$$\mathbf{C}_{4} = (0, a, 0)^{T}$$

T

Frenet-Serret formulae: example

Finally, A circular helix of arc length parametrization is

$$\mathbf{r} = (a \cos \frac{s}{c}, a \sin \frac{s}{c}, \frac{bs}{c})^T$$



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